



Sin -wave oscillators



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Loop gain and phase

$$(U_{in} + \beta U_{out})A_V(U) = U_{out}$$

$$U_{out} = \frac{A_V(U)}{1 - A_V(U)\beta} U_{in}$$

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Oscillations - positive feedback (Barkhausen's criterion)

$$U_{out} = \frac{A_V(U)}{1 - A_V(U)\beta}$$

$$1 = A_V(U)\beta = |A_V(U)\beta|e^{j(\varphi_A + \varphi_\beta)}$$

$|A_V(U)\beta|=1$ **AMPLITUDE condition**

$\varphi_A + \varphi_\beta = n \cdot 360^\circ$ **PHASE condition (n=0,1,2,..)**

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Phase and Amplitude conditions

$|A_V(U)\beta|=1$

$\varphi_A + \varphi_\beta(f) = n \cdot 360$

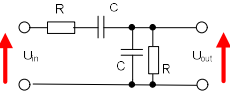
usually $|A_V(U)\beta| > 1$
 U increases $\rightarrow A_V(U)$ decreases
 so:
 amplitude of oscillation is limited

so:
 frequency of oscillation is adjusted



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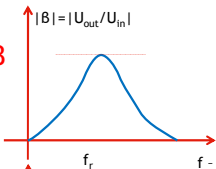
Wien-bridge oscillator



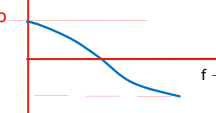
$1/3$

$f_r = \frac{1}{2\pi RC}$


$|B| = |U_{out}/U_{in}|$



90°

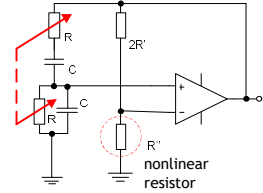


-90°



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Wien oscillator



$f_r = \frac{1}{2\pi RC}$

$|A_V(U)| = \frac{2R'}{R'(U)} + 1 \approx 3$

nonlinear resistor



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Wien oscillator - automatic gain control

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Twin-T filter

$f_r = \frac{1}{2\pi RC}$

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Twin-T oscillator

$\frac{R_2}{R_1} = 10 \dots 1000$

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Phase-Shift oscillators

$\varphi_B = 180^\circ$ $A_V > 30$

$$f_r = \frac{1}{2\pi RC\sqrt{6}}$$

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Phase-Shift oscillators

$\varphi_B = 180^\circ$ $A_V > 30$

$$f_r = \frac{1}{2\pi RC\sqrt{6}}$$

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LC oscillators resonant circuit (serial)

$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

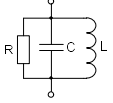
$$Q = \frac{f_0}{\Delta f} = \frac{\omega_0 L}{r}$$

Magnitude response: $|Z/r|$ vs f [log]. Resonance at f_0 .

Phase response: vs f [Hz]. Phase shifts from 90° to -90° .

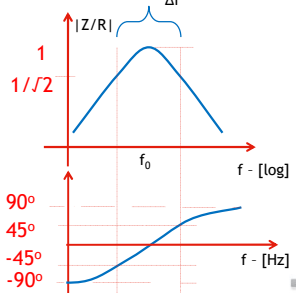
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LC oscillators resonant circuit (parallel)



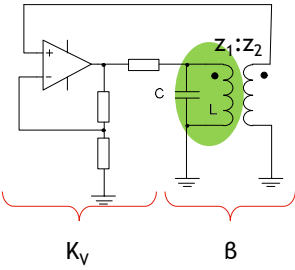
$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

$$Q = \frac{f_0}{\Delta f} = \frac{R}{1/\omega_0 C}$$



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Meissner (Armstrong) oscillator



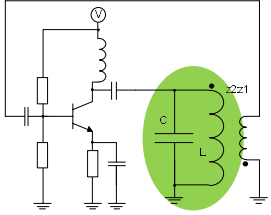
$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

$$\beta(f_0) = \frac{z_1}{z_2}$$

$$A_{Vmin} = \frac{z_2}{z_1}$$

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MEISSNER



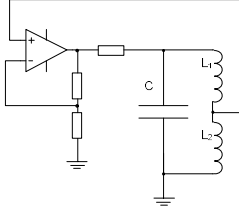
$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

$$\beta(f_0) = \frac{z_1}{z_2}$$

$$A_{Vmin} = \frac{z_2}{z_1}$$

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Hartley oscillator



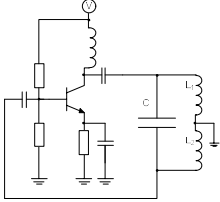
$$f_0 = \frac{1}{2\pi\sqrt{(L_1+L_2)C}}$$

$$\beta(f_0) = \frac{L_2}{L_1 + L_2}$$

$$K_{Vmin} = \frac{L_1 + L_2}{L_2}$$

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Hartley oscillator



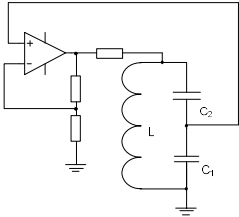
$$f_0 = \frac{1}{2\pi\sqrt{(L_1+L_2)C}}$$

$$\beta(f_0) = \frac{L_2}{L_1 + L_2}$$

$$A_{Vmin} = \frac{L_1 + L_2}{L_2}$$

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Colpitts oscillator



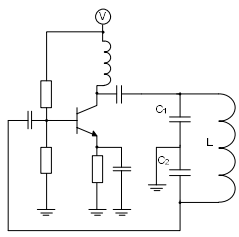
$$f_0 = \frac{1}{2\pi\sqrt{L\frac{C_1C_2}{C_1+C_2}}}$$

$$\beta(f_0) = \frac{C_2}{C_2 + C_1}$$

$$A_{Vmin} = \frac{C_2 + C_1}{C_2}$$

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Colpitts oscillator



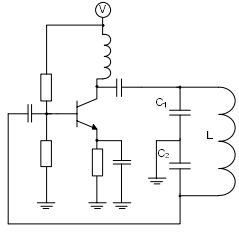
$$f_0 = \frac{1}{2\pi \sqrt{L \frac{C_1 C_2}{C_1 + C_2}}}$$

$$\beta(f_0) = \frac{C_2}{C_2 + C_1}$$

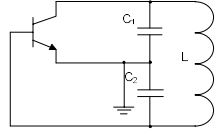
$$A_{vmin} = \frac{C_2 + C_1}{C_2}$$

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Colpitts oscillator



CE

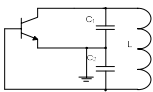


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CE, CC, CB amps in oscillators

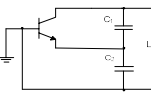
CE

Grounded E



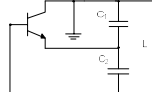
CB

Grounded B



CC

Grounded C



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FET amps as oscillators CG, CD, CS

CG

CD

CS

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Clapp oscillator

$$f_0 = \frac{1}{2\pi\sqrt{LC}}$$

$$\frac{1}{C} = \frac{1}{C_1} + \frac{1}{C_2} + \frac{1}{C_3}$$

$$\beta(f_0) = \frac{C_2}{C_2 + C_1}$$

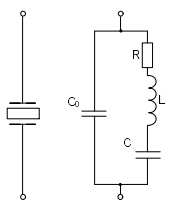
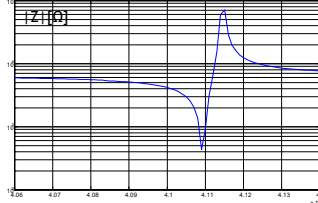
$$A_{Vmin} = \frac{C_2 + C_1}{C_2}$$

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Quartz (crystal) oscillator Clapp

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Crystal equivalent circuit

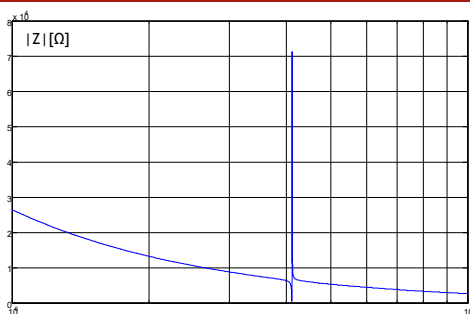



f [Hz]	100 k	500 k	1 M	4 M	10 M	20 M	60 M	120 M
R [Ω]	400	500	250	100	20	10	30	50
L [H]	93,8	20,3	3,62	0,100	0,0169	0,0042	0,0035	0,00293
C [pF]	0,027	0,005	0,007	0,015	0,015	0,015	0,002	0,0006
C ₀ [pF]	6	6	5	5	3,5	3	5	4

Q=25e3

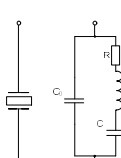
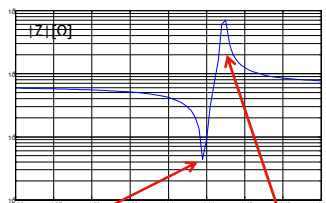
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|Z(f)|



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Series and Parallel resonance of a crystal resonator of 4MHz

Q = 25000

$$f_s = \frac{1}{2\pi\sqrt{LC}}$$

$$f_p = \frac{1}{2\pi\sqrt{L\frac{CC_0}{C+C_0}}}$$

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fs - $|z| = \min$

fp - $|z| = \max$

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series resonans

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Pierce oscillator - an example

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Frequency stability

$f_0(t) = f_0 \pm \Delta f_0$

$$S = \frac{\Delta f_0}{f_0} / 24h$$

Type of oscillator	Stability
RC	10e-2 - 10e-3
LC	10e-3 - 10e-4
Crystal	10e-6 - 10e-7
Crystal (temp. stab.)	(10e-8 - 10e-10)
Atomic references	10e-12 - 10e-14

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Features of oscillators

- frequency range
- frequency stability
- harmonics (THD)
- amplitude and phase noise (jitter)

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Summary

- amplitude and phase conditions of oscillation
 - Wien bridge generator
 - Twin - T filter and oscillator
 - RC phase shifter oscillators
- Meissner, Hartley, Colpits oscillators - topologies
- crystal (quartz) - parallel and series resonances, model, $|Z(f)|$ -graph
- frequency stability and other parameters of generators



Flip-Flops and multivibrators



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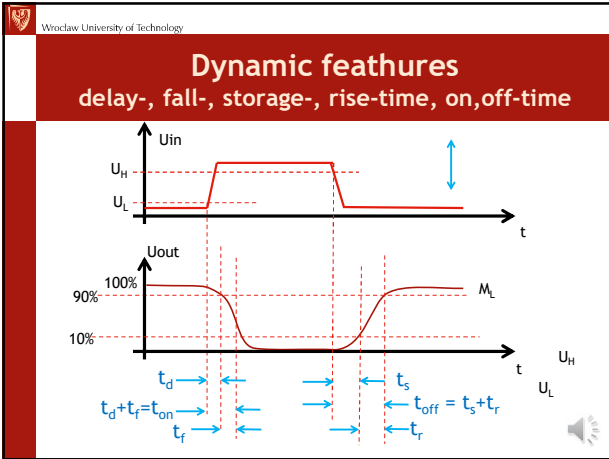
BJ-Transistor as a switch

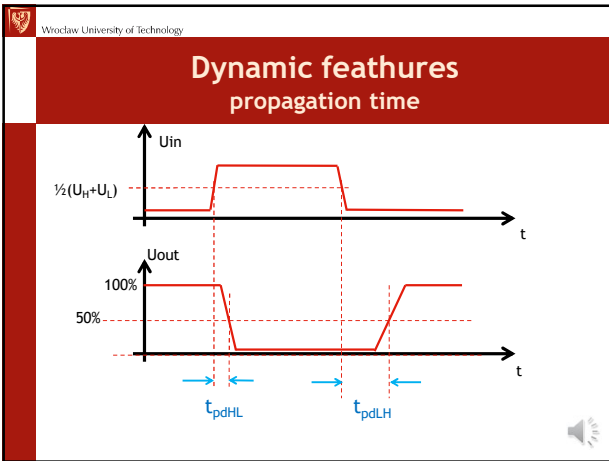
The diagram illustrates a BJT switch circuit. The input voltage U_{in} is applied to the base through a resistor R_B . The collector is connected to V_{CC} through a resistor R_C . The output voltage U_{out} is taken from the collector. The transfer characteristic graph shows U_{out} on the y-axis and U_{in} on the x-axis. The output is high (V_{CC}) for $U_{in} < U_L$ and low ($0.1-1V$) for $U_{in} > U_H$. The transition region is between U_L and U_H . The high-level gain is M_H and the low-level gain is M_L .

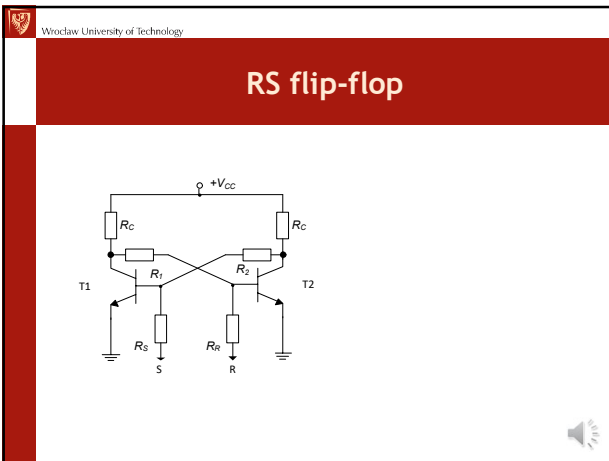
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MOSFE-Transistor as a switch

The diagram illustrates a MOSFET switch circuit. The input voltage U_{in} is applied to the gate through a resistor R_B . The drain is connected to V_{CC} through a resistor R_C . The output voltage U_{out} is taken from the drain. The transfer characteristic graph shows U_{out} on the y-axis and U_{in} on the x-axis. The output is high (V_{CC}) for $U_{in} < U_L$ and low ($0.01-1V$) for $U_{in} > U_H$. The transition region is between U_L and U_H . The high-level gain is M_H and the low-level gain is M_L . The threshold voltage U_{TH} is indicated as $0.6-3V$.







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Astable Flip-Flop

$t_1 \approx 0.7R_1C_1$ $t_2 \approx 0.7R_2C_2$
 $R_C \ll R_1, R_2 \ll \beta R_C$

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OpAmp(Comparator) Flip-Flop

$T = 2R_1C \ln \frac{1+\beta}{1-\beta}$
 $\beta = \frac{R_3}{R_2 + R_3}$

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Astable Flip-Flop with NAND Gate

$f = \frac{1}{t_1 + t_2} = \frac{1}{R_1C_1 + R_2C_2}$

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Timer „555” - monostable mode

$T = \ln 3 \cdot RC$

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Timer „555” - astable mode

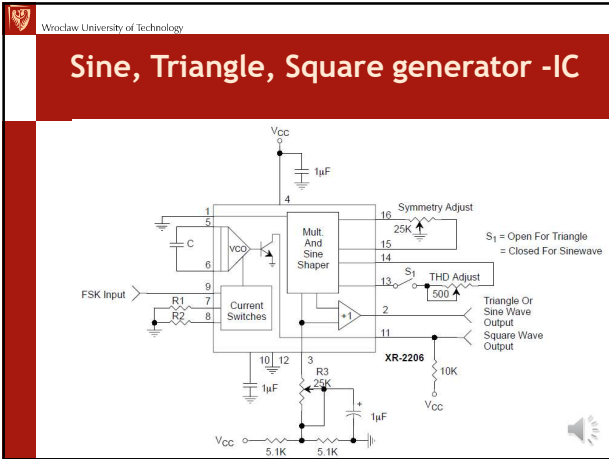
$f = \frac{1}{T} = \frac{1}{\ln(2)(R_A + 2R_B)C}$

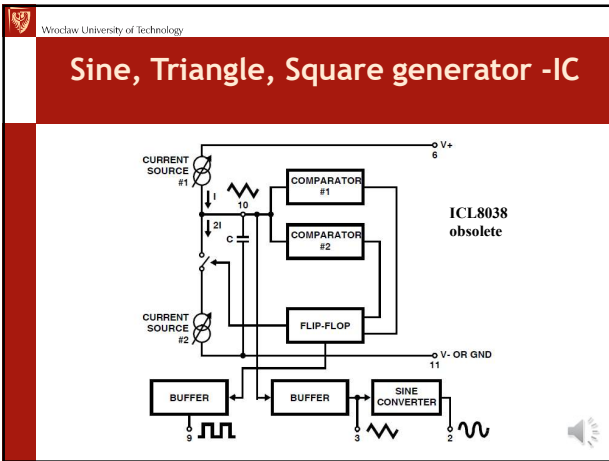
$D = \frac{t_1}{T} = \frac{R_A + R_B}{R_A + 2R_B}$

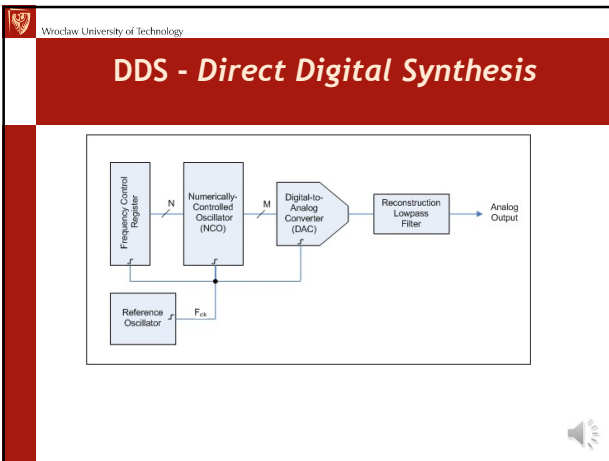
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VCO F-F - Emmitter coupling

$f = \frac{I}{4U_{BE}C}$







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DDS - Direct Digital Synthesis

Components: Except as indicated, standard values of components and in manufacturing quantities are in accordance with IEC standards and are shown in IEC units. www.farnell.com

Outlines Model:
 Model of the daughtercard is available in the form of a 3D model (STEP, IGS, STL, etc.) in the folder "3D Model" of the project.

DDS-69 Daughtercard
 Rev. 01.00, 14. 02.05
 NDAPB, NDXX

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Summary

- Phase and amplitude conditions of oscillations
- Flip-Flop as a-stable and mono-stable
- Timer 555
- Function generator
- DDS generator
