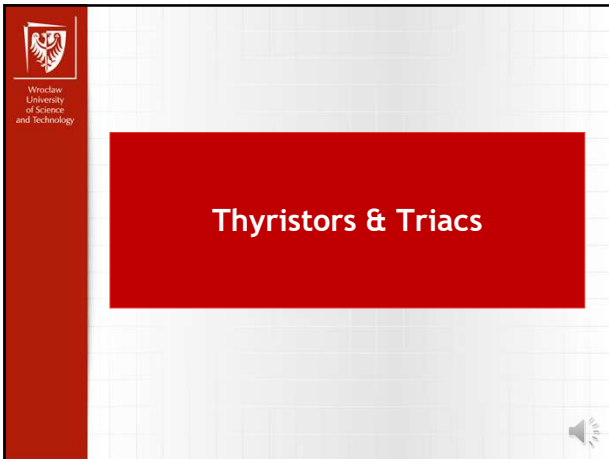
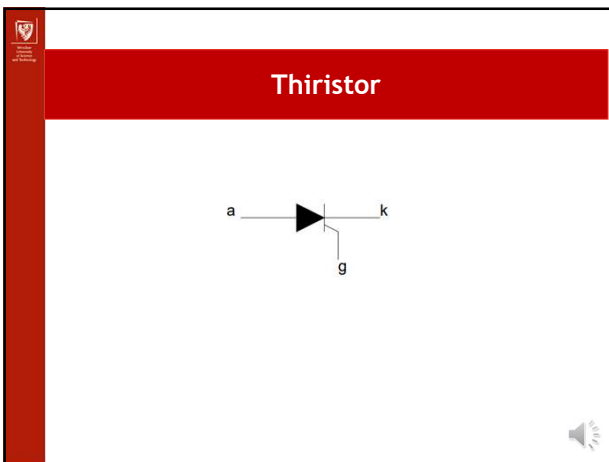
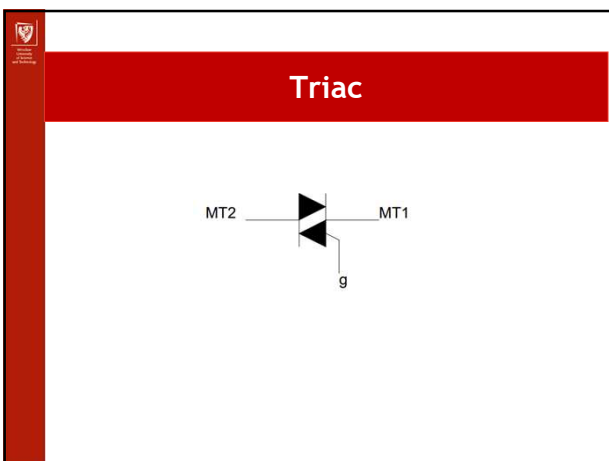
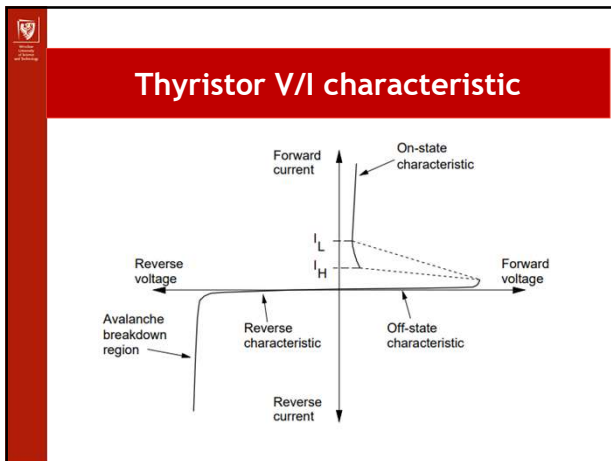
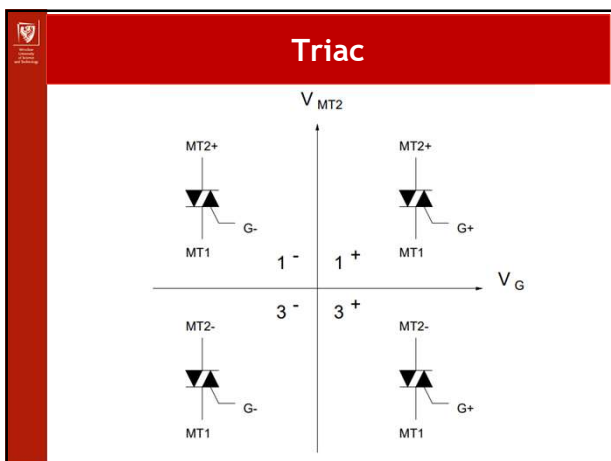


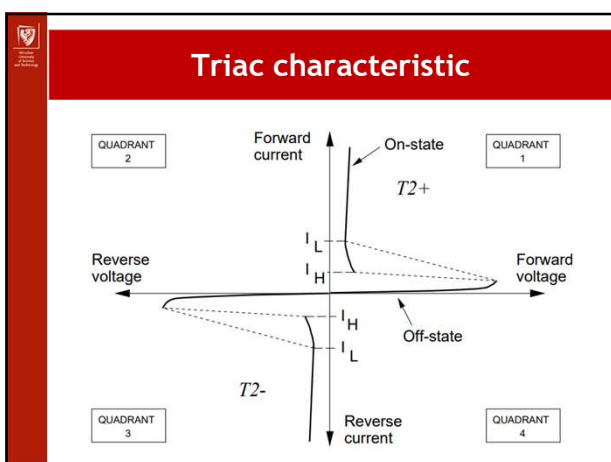












Rule 1:
To turn a thyristor (or triac) ON, a gate current $\geq I_{GT}$ must be applied until the load current is $\geq I_L$.
This condition must be met at the lowest expected operating temperature.

Rule 2:
To turn off (commutate) a thyristor (or triac), the load current must be $< I_H$ for sufficient time to allow a return to the blocking state.
This condition must be met at the highest expected operating temperature.

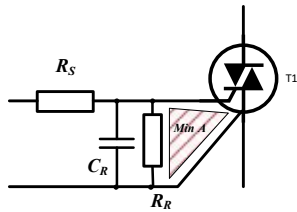
BT139-600 parameters					
Static characteristics					
I_{GT}	gate trigger current	$V_D = 12\text{ V}; I_T = 0.1\text{ A}; T_2+ G+;$ $T_J = 25^\circ\text{C}; \text{Fig. 7}$	-	5	35 mA
		$V_D = 12\text{ V}; I_T = 0.1\text{ A}; T_2+ G-;$ $T_J = 25^\circ\text{C}; \text{Fig. 7}$	-	8	35 mA
		$V_D = 12\text{ V}; I_T = 0.1\text{ A}; T_2- G-;$ $T_J = 25^\circ\text{C}; \text{Fig. 7}$	-	10	35 mA
		$V_D = 12\text{ V}; I_T = 0.1\text{ A}; T_2- G+;$ $T_J = 25^\circ\text{C}; \text{Fig. 7}$	-	22	70 mA
I_L	latching current	$V_D = 12\text{ V}; I_G = 0.1\text{ A}; T_2+ G+;$ $T_J = 25^\circ\text{C}; \text{Fig. 8}$	-	7	40 mA
		$V_D = 12\text{ V}; I_G = 0.1\text{ A}; T_2+ G-;$ $T_J = 25^\circ\text{C}; \text{Fig. 8}$	-	20	60 mA
		$V_D = 12\text{ V}; I_G = 0.1\text{ A}; T_2- G-;$ $T_J = 25^\circ\text{C}; \text{Fig. 8}$	-	8	40 mA
		$V_D = 12\text{ V}; I_G = 0.1\text{ A}; T_2- G+;$ $T_J = 25^\circ\text{C}; \text{Fig. 8}$	-	10	60 mA
I_H	holding current	$V_D = 12\text{ V}; T_J = 25^\circ\text{C}; \text{Fig. 9}$	-	6	45 mA

Dynamic BT139 parameters						
dV_{CE}/dt	rate of rise of off-state voltage	$V_{CEM} = 402\text{ V}$; $T_J = 125^\circ\text{C}$; ($V_{CEM} = 67\%$ of V_{CEM}), exponential waveform; gate open circuit	200	250	-	V/ μs
dV_{CEM}/dt	rate of change of commutating voltage	$V_D = 400\text{ V}$; $T_J = 95^\circ\text{C}$; $dI_{GSM}/dt = 7.2\text{ A/ms}$; $I_T = 16\text{ A}$; gate open circuit	10	20	-	V/ μs
t_{gt}	gate-controlled turn-on time	$I_{TM} = 20\text{ A}$; $V_D = 600\text{ V}$; $I_G = 0.1\text{ A}$; $dI_G/dt = 5\text{ A}/\mu\text{s}$	-	2	-	μs

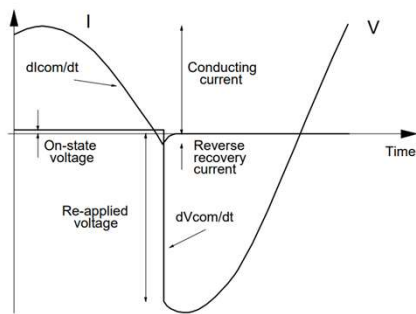
BT139-600 parameters	
Rule 3:	When designing a triac triggering circuit,
	avoid triggering in the 3+ quadrant (MT2-, G+) where possible

Unwanted commutation	
Rule 4:	To minimise noise pickup, keep gate connection length to a minimum. Take the return directly to MT1 (or cathode). If hard wired, use twisted pair or shielded cable. Fit a resistor of $1\text{ k}\Omega$ or less between gate and MT1. Fit a bypass capacitor in conjunction with a series resistor to the gate. Alternatively, use an insensitive series H triac

Reduction of noise in gate loop



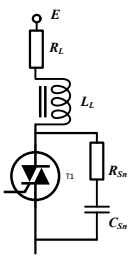
Unwanted commutation Triac dV_{COM}/dt



Dynamic BT139 parameters

dV_G/dt	rate of rise of off-state voltage	$V_{DM} = 402\text{ V}$; $T_J = 125^\circ\text{C}$; ($V_{DM} = 67\%$ of V_{DRM}), exponential waveform; gate open circuit	200	250	-	V/ μs
dV_{COM}/dt	rate of change of commutating voltage	$V_D = 400\text{ V}$; $T_J = 95^\circ\text{C}$; $dI_{COM}/dt = 7.2\text{ A/ms}$; $I_T = 16\text{ A}$; gate open circuit	10	20	-	V/ μs
t_{gt}	gate-controlled turn-on time	$I_{TM} = 20\text{ A}$; $V_D = 600\text{ V}$; $I_G = 0.1\text{ A}$; $dI_G/dt = 5\text{ A}/\mu\text{s}$	-	2	-	μs

$dV_{com}/dt = (dV/dt)_{com}$

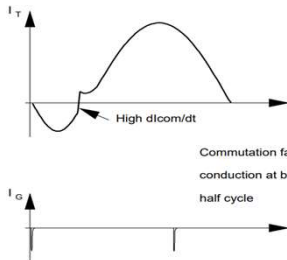


$$C_{Sn} \approx (1 - 4) * \left(\frac{E^2}{L_L * \left(\frac{dV}{dt} \right)_c^2} \right)$$

$$R_{Sn} \approx (1 - 2) * \left(\sqrt{\frac{L_L}{C_{Sn}}} - R_L \right)$$

$$P_{R_{Sn}} \approx C_{Sn} E^2 f_s$$

**Unwanted commutation
Triac dI_{com}/dt**



Commutation failure causes
conduction at beginning of
half cycle

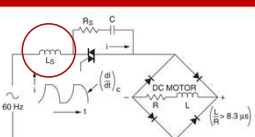
no benefit in adding a snubber across the triac
because dV_{com}/dt is not the problem.....

T5035H-8PI

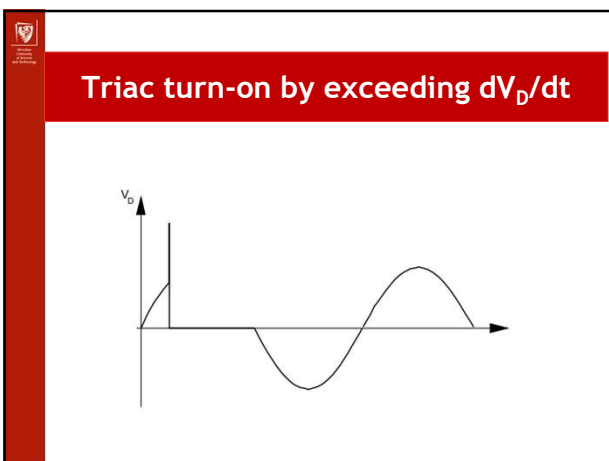
Symbol	Test conditions	Quadrants		Value	Unit	
I_{GT}	$V_D = 12 \text{ V}, R_L = 30 \Omega$	I - II - III	Min.	5	mA	
	$V_D = 12 \text{ V}, R_L = 30 \Omega$	I - II - III	Max.	35	mA	
V_{GT}	$V_D = 12 \text{ V}, R_L = 30 \Omega$	I - II - III	Max.	1.3	V	
V_{GD}	$V_D = V_{DRM}, R_L = 3.3 \text{ k}\Omega$	I - II - III	Min.	0.15	V	
I_L	$I_G = 1.2 \times I_{GT}$	I - III	Max.	75	mA	
		II	Max.	90	mA	
$I_H^{(1)}$	$I_T = 500 \text{ mA}$, gate open		Max.	60	mA	
$dV/dt^{(1)}$	$V_D = 536 \text{ V}$, gate open		$T_J = 150^\circ\text{C}$	Min.	2000	V/ μs
$(dI/dt)^{(1)}$	Without snubber network		$T_J = 150^\circ\text{C}$	Min.	40	A/ms

1. For both polarities of A2 referenced to A1.

di_{com}/dt	rate of change of commutating current	$V_D = 400\text{ V}; T_J = 150^\circ\text{C}; I_{T(RMS)} = 16\text{ A}; dV_{com}/dt = 20\text{ V}/\mu\text{s}; \text{gate open circuit; snubberless condition}$		12	-	-	A/ms
		$V_D = 400\text{ V}; T_J = 150^\circ\text{C}; I_{T(RMS)} = 16\text{ A}; dV_{com}/dt = 10\text{ V}/\mu\text{s}; \text{gate open circuit}$		15	-	-	A/ms
		$V_D = 400\text{ V}; T_J = 150^\circ\text{C}; I_{T(RMS)} = 16\text{ A}; dV_{com}/dt = 1\text{ V}/\mu\text{s}; \text{gate open circuit}$		20	-	-	A/ms



no benefit in adding a snubber across the triac because dV_{COM}/dt is not the problem....add L_s [a few mH can be saturated].



Dynamic BT139 parameters

dV_{D}/dt	rate of rise of off-state voltage	$V_{DM} = 402\text{ V}$; $T_J = 125\text{ }^{\circ}\text{C}$; ($V_{DM} = 67\%$ of V_{DRM}); exponential waveform; gate open circuit	200	250	-	V/ μs
dV_{GS}/dt	rate of change of commutating voltage	$V_D = 400\text{ V}$; $T_J = 95\text{ }^{\circ}\text{C}$; $dI_{GS}/dt = 7.2\text{ A/ms}$; $I_T = 16\text{ A}$; gate open circuit	10	20	-	V/ μs
t_{gt}	gate-controlled turn-on time	$I_{TM} = 20\text{ A}$; $V_D = 600\text{ V}$; $I_G = 0.1\text{ A}$; $dI_G/dt = 5\text{ A}/\mu\text{s}$	-	2	-	μs

Snubber; L[mH]; filter

T5035H-8PI

Symbol	Test conditions	Quadrants		Value	Unit
I_{GT}	$V_D = 12\text{ V}$, $R_L = 30\text{ }\Omega$	I - II - III	Min.	5	mA
	$V_D = 12\text{ V}$, $R_L = 30\text{ }\Omega$	I - II - III	Max.	35	mA
V_{GT}	$V_D = 12\text{ V}$, $R_L = 30\text{ }\Omega$	I - II - III	Max.	1.3	V
V_{GD}	$V_D = V_{DRM}$, $R_G = 3.3\text{ k}\Omega$	I - II - III	Min.	0.15	V
I_L	$I_G = 1.2 \times I_{GT}$	I - III	Max.	75	mA
		II	Max.	90	mA
$I_H^{(1)}$	$I_T = 500\text{ mA}$, gate open		Max.	60	mA
$dV/dt^{(1)}$	$V_D = 536\text{ V}$, gate open	$T_J = 150\text{ }^{\circ}\text{C}$	Min.	2000	V/ μs
$(di/dt)^{(1)}$	Without snubber network	$T_J = 150\text{ }^{\circ}\text{C}$	Min.	40	A/ms

1. For both polarities of A2 referenced to A1.

T5035H-8PI

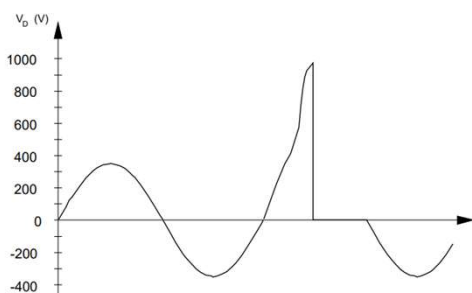
- 50 A RMS Snubberless Triac
- 800 V symmetrical blocking voltage
- 150 °C maximum junction temperature T_j
- Three triggering quadrants
- High noise immunity - static dV/dt
- Robust dynamic turn-off commutation - $(dl/dt)_c$

Rule 5:

Where high dV_D/dt or dV_{COM}/dt are likely to cause a problem, fit an RC snubber across MT1 and MT2.

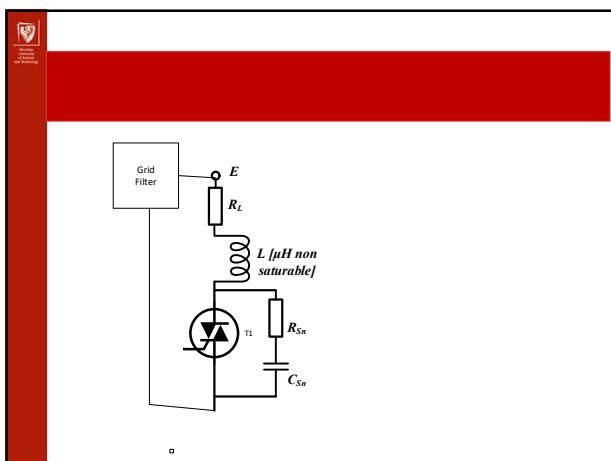
Where high dl_{COM}/dt is likely to cause a problem, fit an inductor of a few mH (saturated !?) in series with the load. Alternatively, use a Hi-Com triac

Triac turn-on by exceeding V_{DRM}



BT139

Symbol	Parameter	Conditions	Min	Max	Unit
V_{DRM}	repetitive peak off-state voltage		-	600	V



di_T/dt - burn out

Rule 6.
If the triac's V_{DRM} is likely to be exceeded during severe mains transients, employ one of the following measures:

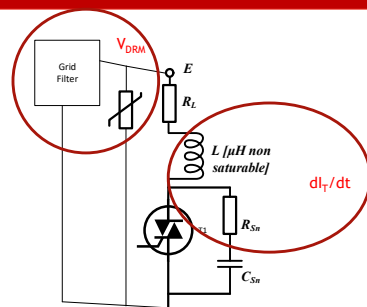
- Limit high di_T/dt with a non saturable inductor of a few μH in series with the load;
- Use a MOV (Metal Oxide Varistor) across the mains in combination with filtering on the supply side

di_T/dt prevent

Rule 8:

If the triac's di_T/dt is likely to be exceeded, an air cored inductor of a few μH or an NTC thermistor should be fitted in series with the load.

Alternatively, employ zero voltage turn-on for resistive loads.



Rule 7:

Healthy gate drive and avoiding 3+ (IV quadrant) operation maximises the triac's di_T/dt capability.

BT139

di/dt	rate of rise of on-state current	I _T = 20 A; I _G = 0.2 A; di _G /dt = 0.2 A/μs; T2+ G+			A/μs
		I _T = 20 A; I _G = 0.2 A; di _G /dt = 0.2 A/μs; T2+ G-	-	50	A/μs
		I _T = 20 A; I _G = 0.2 A; di _G /dt = 0.2 A/μs; T2- G-	-	50	A/μs
		I _T = 20 A; I _G = 0.2 A; di _G /dt = 0.2 A/μs; T2- G+	-	10	A/μs

Rule 9:
 Avoid mechanical stress to the triac when fitting it to the heatsink.
 Fix, then solder.
 Never pop rivet with the rivet mandrel on the tab side.

Rule 10:
 For longterm reliability, ensure that the R_{th j-a} is low enough to keep the junction temperature within T_j max for the highest expected ambient temperature.

$$R_{th\ j-a} = R_{th\ j-mb} + R_{th\ mb-h} + R_{th\ h-a} \quad [K/W]$$



Test problems

- Prąd załączania (gate current I_{GT})
- Prąd włączania (latch current I_L)
- Prąd wyłączania (holding current I_H)
- Niekontrolowane włączenia triaka:
 - Szumy w obwodzie bramki (odfiltrować i zbocznikować bramkę)
 - Przekroczenie dV_{COM}/dt (w czasie wyłączania obc. indukcyjnego - snubber)
 - Przekroczenie dI_{COM}/dt (nieoczekiwane wyłączenie prądu - indukcyjność uH bez nasycenia)
 - Przekroczenie chwilowe dV_o/dt (bez przekroczenia trwałego V_{DRM} - filtracja sieci; MOV)
 - Chwilowe przekroczenie V_{DRM} (powtarzalne - filtracja sieci; MOV)
- Rola układu tłumiącego (snubber)
